

Investigation of adjoint method inverse design applied to fiber-to- chip edge coupling

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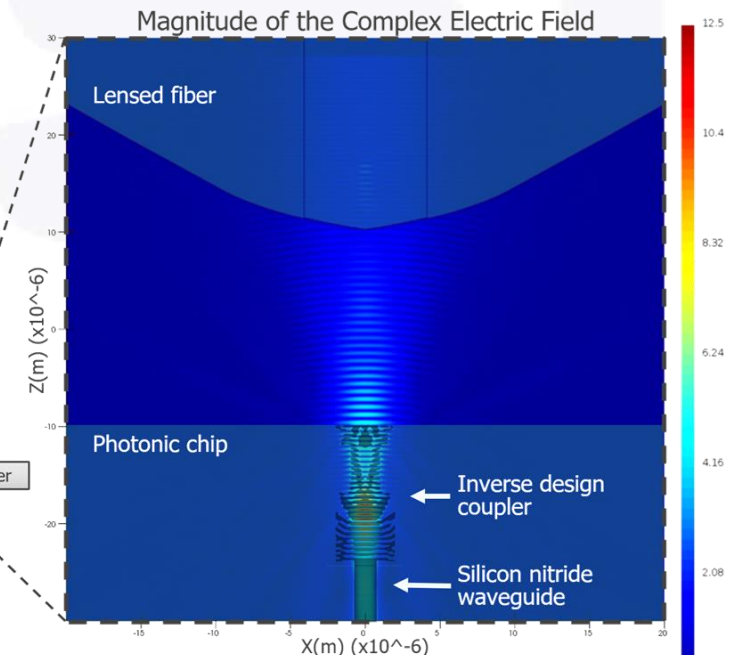
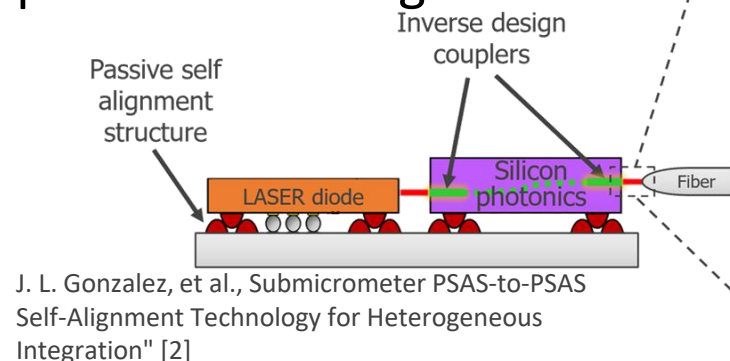
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PA #: AFRL - 2024 - 5983

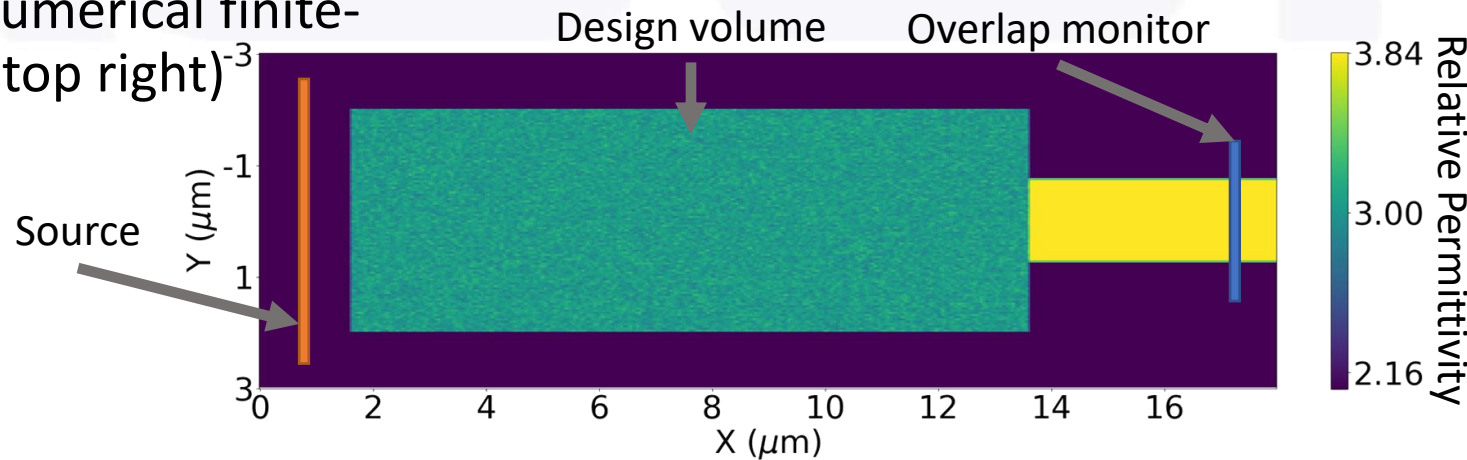
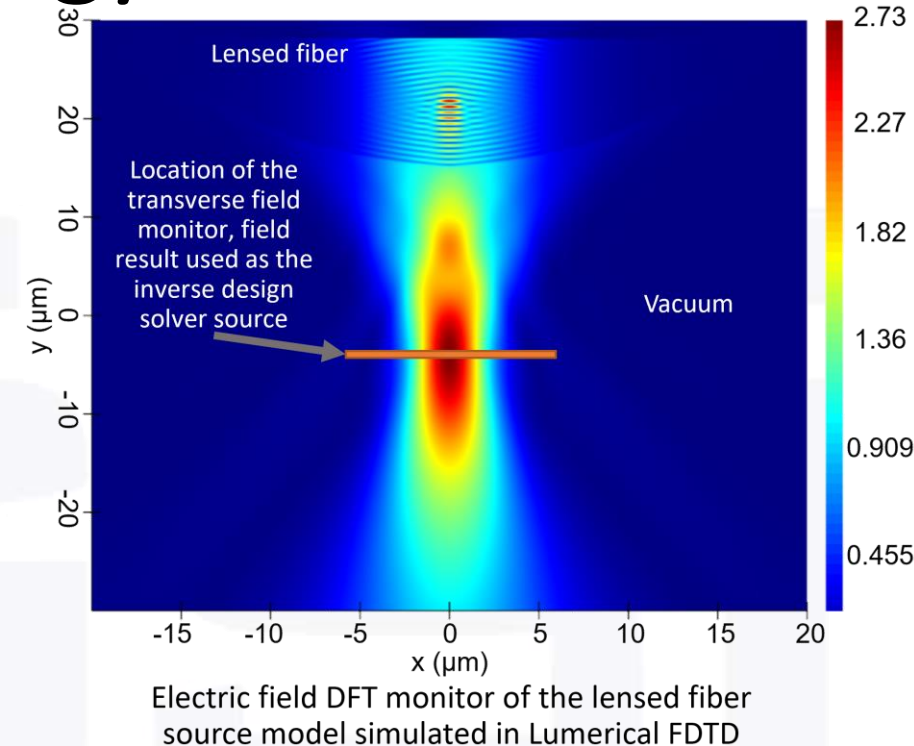
Background and Motivation

- Full-vectorial electromagnetic modeling of nanophotonic components on large simulation domains ($> 1000 \lambda^3$) is computationally complex
 - Solvers incorporating GPU accelerated hardware have mitigated computation time challenges in finite-difference EM modeling
- Leveraging this capability, inverse design edge couplers are optimized, fabricated, and characterized in a study to:
 1. Reduce the footprint of typical photonic edge couplers for the silicon nitride on insulator material platform
 2. Understand the performance tradeoffs of inverse design
 3. Determine if inverse design is a viable design methodology for future projects and research in photonic heterogeneous integration [1]



Edge Coupler Design Methodology

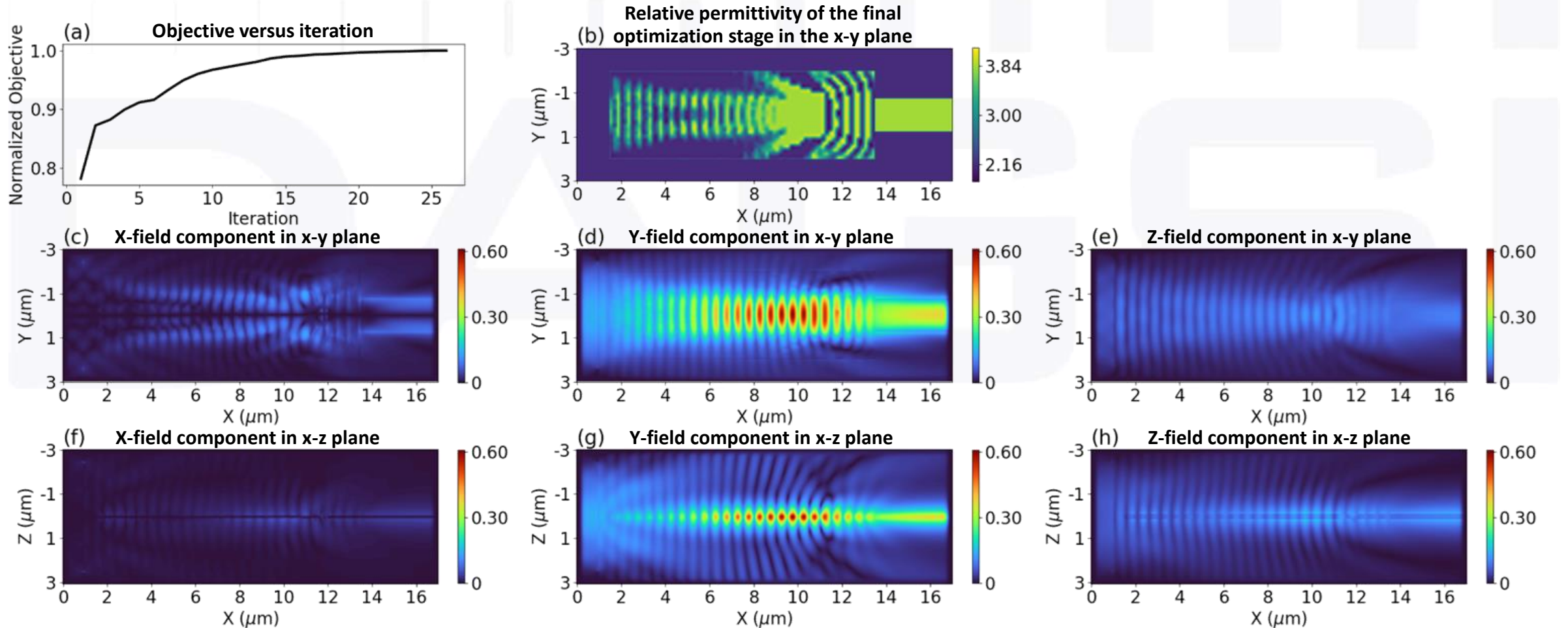
- In-plane lensed fiber-to-chip coupling adjoint method inverse design in SPINS-b [3]
 - Finite-difference frequency-domain (FDFD) solver
 - Randomly pixelated $12.0 \times 4.0 \times 0.04 \mu\text{m}$ design region (bottom right plot)
 - $17 \times 6 \times 6 \mu\text{m}$ computational domain with 40 nm grid spacing and PML absorbing boundary condition (9.69M grid cells)
 - $6.4 \mu\text{m}$ S-polarized spot size source placed at the component facet; source mode field determined by modeling a lensed fiber in the Lumerical finite-difference time-domain solver (top right)





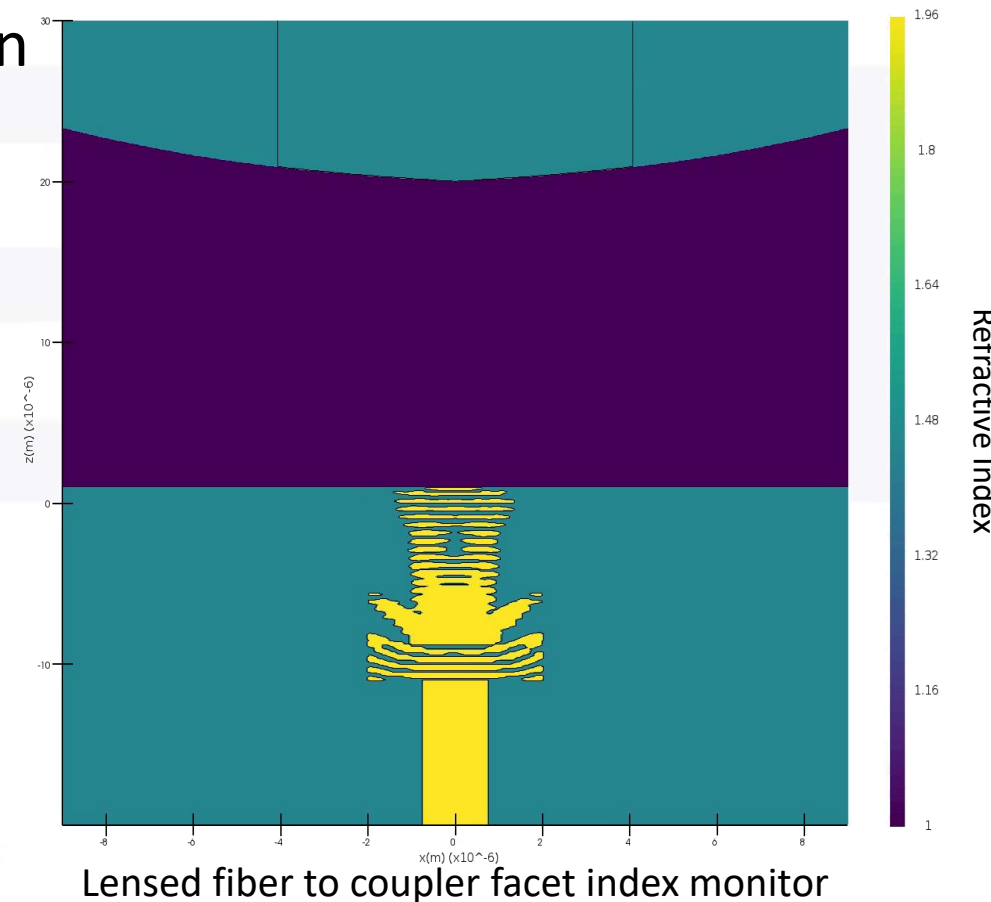
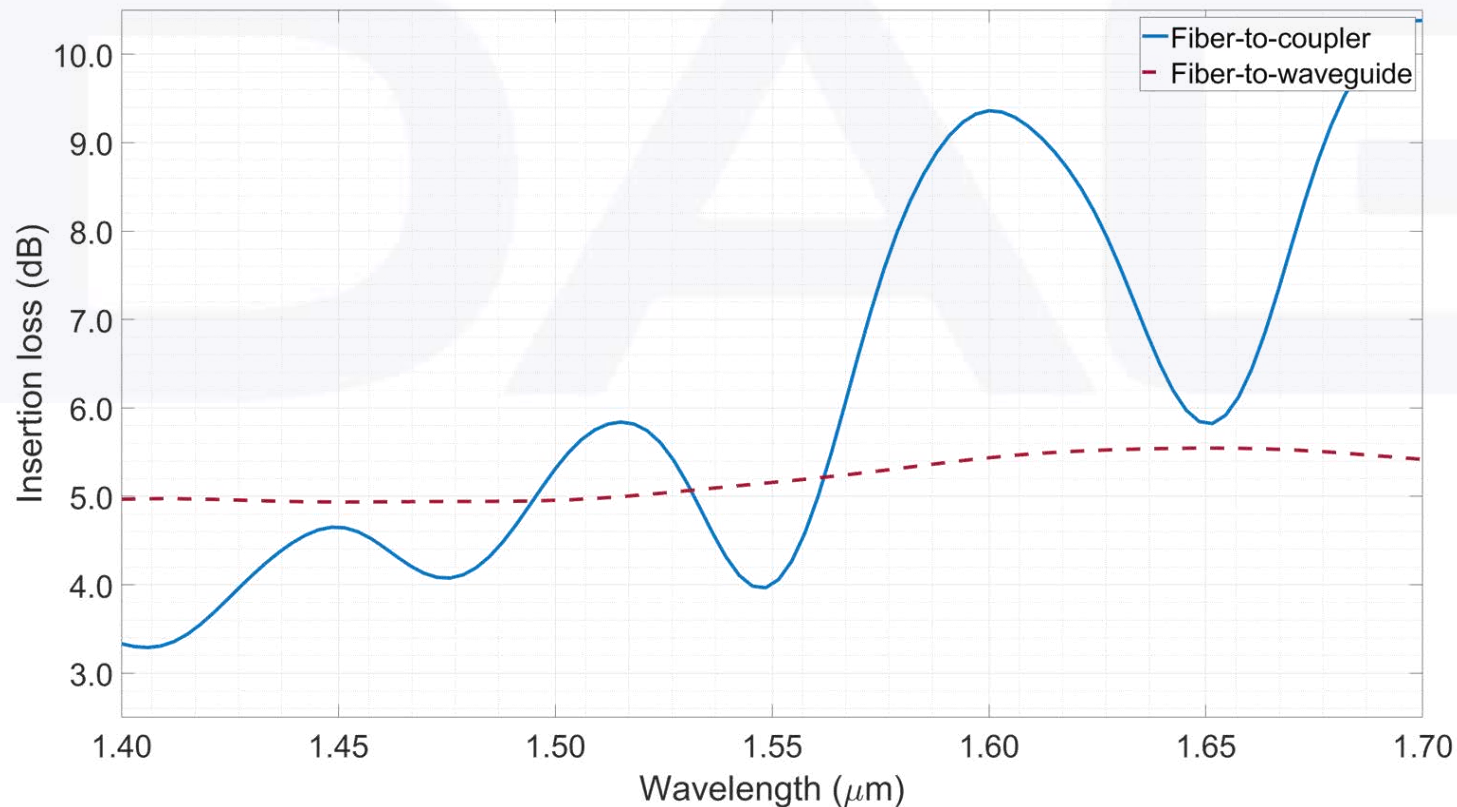
Optimization Results

- Permittivity and FDFD field solution after 26 optimization iterations
- Elapsed computation time: 3 hours



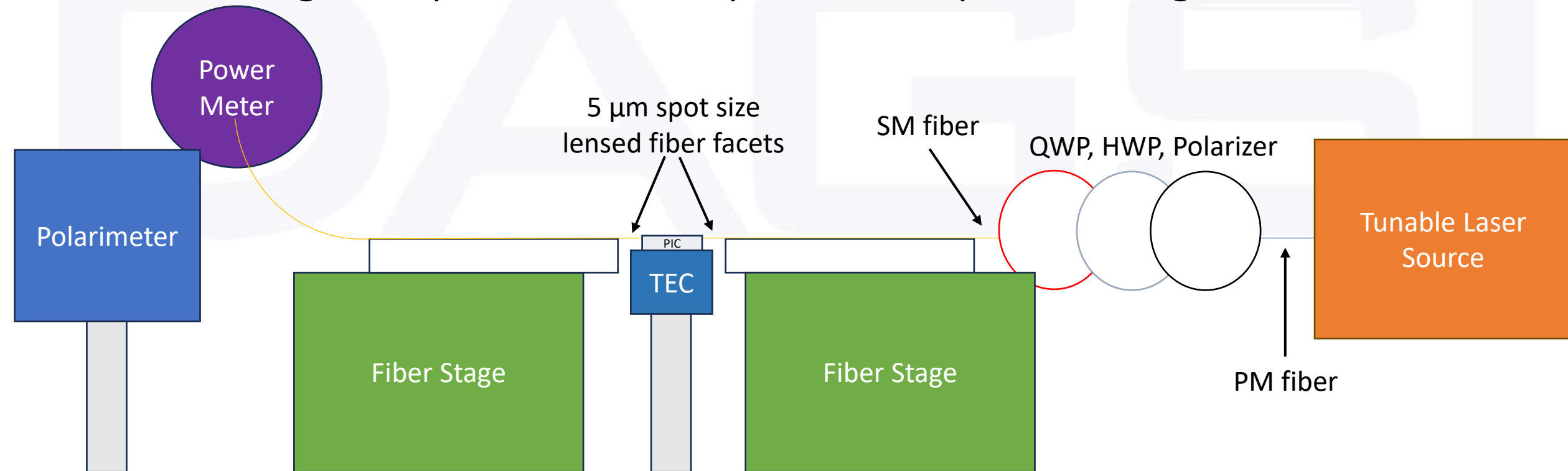
Broadband fiber-to-chip FDTD Validation

- To simulate the coupling loss, the lensed fiber-to-chip coupling experiment was modeled in Lumerical FDTD
- Pulsed source used to extract broadband performance
- 4 dB loss at 1.55 μm in the quasi-TE polarization



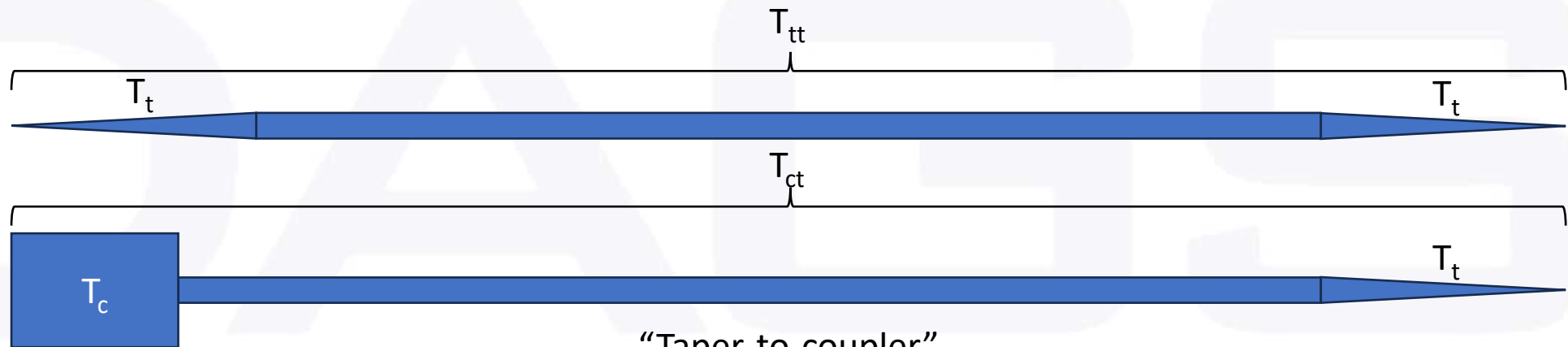
Experimental Setup

- Prior to taking data, the input fiber stage is raised to couple light into the polarimeter for feedback to tune the desired polarization state using the two waveplates
- The couplers are actively aligned to maximize power at $1.55\ \mu\text{m}$, laser wavelength swept between $1.51\ \mu\text{m}$ and $1.63\ \mu\text{m}$ wavelength



Determining Coupling Loss

- Using three measurements: baseline power (measurement excluding PIC), taper-to-taper layout, and taper-to-coupler layout, the transmission of the inverse design coupler can be determined as shown below
- Waveguide loss is negligible for the lengths used in the experiment



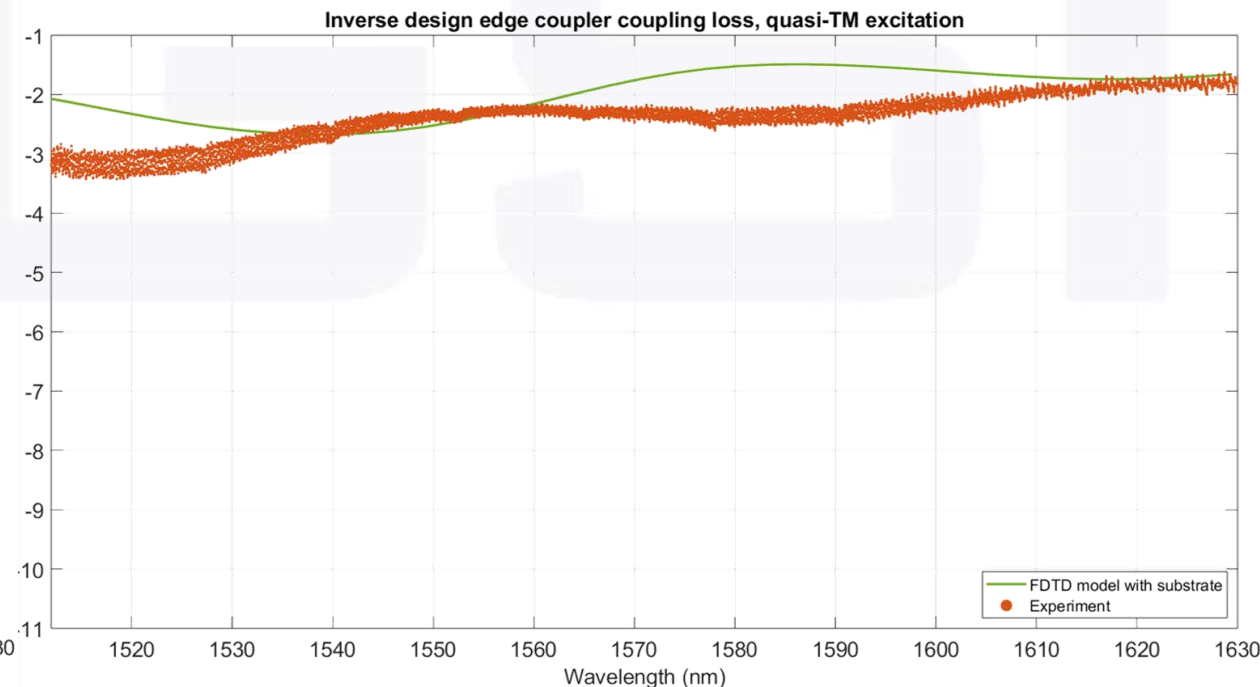
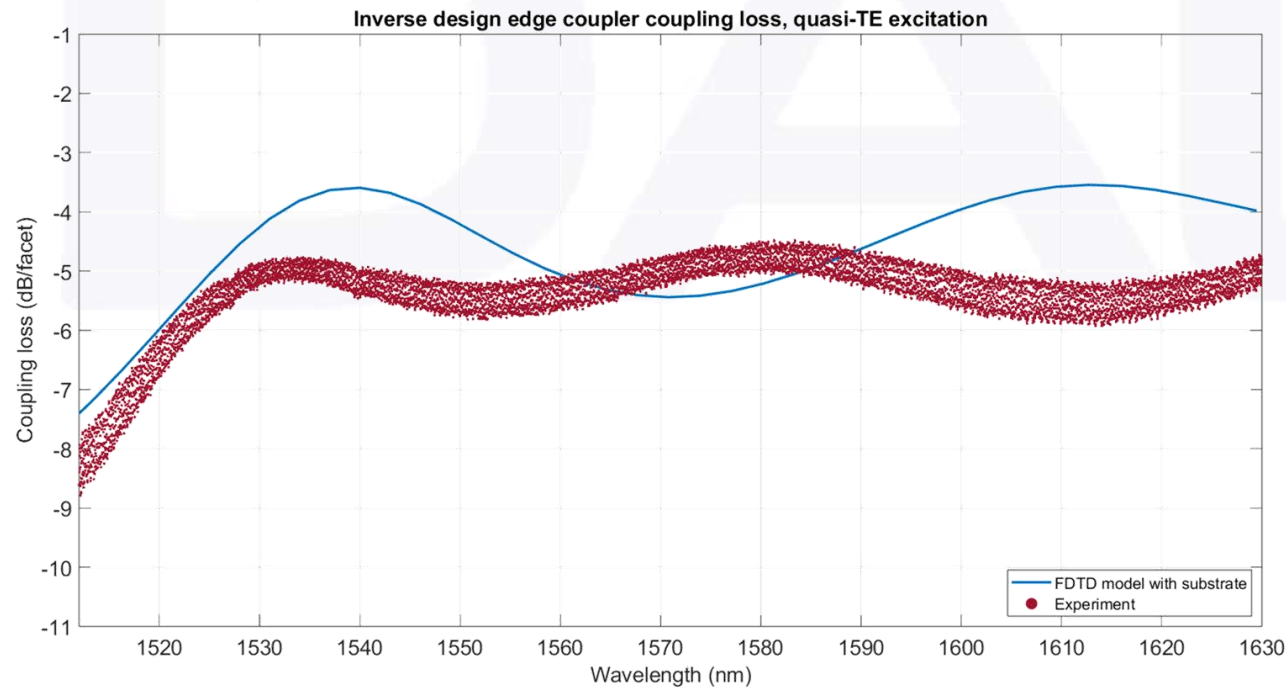
“Taper-to-coupler”

$$T_c(\lambda) = \frac{T_{ct}(\lambda)}{T_t(\lambda)}$$

$$T_c(\lambda)^2 = \left(\frac{P_{ct}(\lambda)}{P_{baseline}(\lambda)} \right)^2 = \frac{P_{ct}(\lambda)^2}{\sqrt{\frac{P_{tt}(\lambda)}{P_{baseline}(\lambda)}} \cdot P_{baseline}(\lambda)}$$

Experimental Results

- Experiments were executed coupling to the quasi-TE and quasi-TM waveguide modes and compared to the FDTD model
- Experimental results show close resemblance to FDTD simulations with losses between 4.8 to 6 dB coupling loss in the quasi-TE polarization and 2.2 to 3.5 dB coupling loss in the quasi-TM polarization throughout the optical C-band



Conclusion

- Design, validation, fabrication, and characterization of inverse design edge couplers was performed to create a compact coupling solution
- Discrepancy between simulation and experiment may be attributed to:
 - Dielectric averaging and grid size in the FDTD model causing a misrepresentation of small features
 - Lithographic patterning feature size limitation
 - Lens shape in model vs. experiment
 - Laboratory environment and model assumptions w.r.t. material parameters
 - Assumptions in the coupling loss calculation
- Quasi-TM polarization showed lower coupling loss compared to quasi-TE in simulation and experiment, suitable for quasi-TM applications where die area is a constraint
- For low-loss applications, coupling can be improved by increasing the fractional area between the coupling mode and design region
 - This may be facilitated by adding more layers vertically or coupling out of plane

References

- [1] Bernard M. Melus, Joseph S. Suelzer, Matt Hagedon, Ronald M. Reano, "Investigation of adjoint method inverse design applied to photonic integrated circuit fiber-to-chip edge couplers," Proc. SPIE 12892, Optical Interconnects XXIV, 1289208 (11 March 2024); <https://doi.org/10.1117/12.3001211>
- [2] J. L. Gonzalez, S. K. Rajan, J. R. Brescia and M. S. Bakir, "A Substrate-Agnostic, Submicrometer PSAS-to-PSAS Self-Alignment Technology for Heterogeneous Integration," in IEEE Transactions on Components, Packaging and Manufacturing Technology, vol. 11, no. 12, pp. 2061-2068, Dec. 2021, doi: 10.1109/TCPMT.2021.3109913.
- [3] Su, L., Vercruysse, D., Skarda, J., Sapra, N. V., Petykiewicz, J. A., and Vuckovic, J., "Nanophotonic inverse design with spins: Software architecture and practical considerations," (2019).